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How to cite: Huaman K, Lozano A, Navarro N, Ortega K. Decolourization of Synthetic Wastewater Related to the Textile Industry Using Photo-Fenton. Textile & Leather Review. 2024; 7:468-480. <https://doi.org/10.31881/TLR.2024.010>

How to link: <https://doi.org/10.31881/TLR.2024.010>

Published: 22 March 2024



Decolourization of Synthetic Wastewater Related to the Textile Industry Using Photo-Fenton

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Article

<https://doi.org/10.31881/TLR.2024.010>

Received 15 January 2024; Accepted 15 March 2024; Published 22 March 2024

ABSTRACT

The artisanal textile industry plays a vital role in the economy by providing a wide variety of products. However, this sector generates large quantities of wastewater containing a diversity of organic compounds, including dyes that, when released into the environment, contribute significantly to water pollution. In this research, samples of synthetic wastewater containing green aniline were subjected to decolourization using the photo-Fenton process. Synthetic textile wastewater was prepared at a concentration of 40 mg/L, and a calibration curve was established. During the treatment, ferrous sulfate (at concentrations of 50 and 150 mg/L) and H₂O₂ (at concentrations of 0.5 and 1.0 g/L) were added to 1 L of the synthetic effluent in a stirring medium (at 1000 rpm) and exposed to solar radiation for 1, 2, or 3 hours, while maintaining a pH of 3. To quantify the degree of decolourization, absorbance was measured at the beginning and end of the treatment using a colourimeter. The optimal conditions for Fe²⁺ concentration, H₂O₂ concentration, and treatment time, with an initial concentration of 40 mg/L, were found to be 150 mg/L, 1.0 g/L, and 3 hours, respectively. Under these conditions, the percentage of decolourization reached 97.546%. The study demonstrated that the concentration of Fe²⁺ and treatment time, as well as the interaction between Fe²⁺ concentration, H₂O₂ concentration, and treatment time, significantly influenced the degree of decolourization. Conversely, the concentration of H₂O₂ and other interactions did not exhibit significant influence.

KEYWORDS

decolorization, synthetic wastewater, textile industry, photo-Fenton

INTRODUCTION

The global textile industry has experienced exponential growth in recent decades, emerging as one of the fastest-expanding manufacturing sectors [1]. This surge is primarily fueled by a sustained increase in demand for textile goods, driven by factors such as demographic growth and consumption patterns. While this growth brings evident economic and social benefits, it also leads to significant environmental damage that cannot be ignored [2].

Moreover, as one of the most water and chemical-intensive sectors, the textile industry produces dyes, which account for approximately 8% to 20% of the total contaminant load, along with auxiliary

chemicals, all dissolved in large volumes of water [3–5]. This poses a severe threat to delicate aquatic ecosystems globally, as both dyes and chemical additives exhibit notable stability and persistence in the environment [6].

On the other hand, wastewater from textile dyes poses significant challenges in decomposition due to its high biochemical oxygen demand (BOD), substantial concentration of dissolved solids, and stable chemical structure [7]. Specifically, nitrogen dyes, such as aniline, possess a complex aromatic structure, limiting the effectiveness of conventional biological treatment methods [8]. Thus, the urgent need to explore and develop treatment alternatives capable of bleaching textile wastewater is emphasized, as also highlighted in various studies [9,10].

Given this context, new technological alternatives, such as advanced oxidation processes (AOP), are imperative, as these unconventional methods are highly effective in degrading toxic or persistent pollutants, thanks to the generation of hydroxyl radicals ($\bullet\text{OH}$) [11]. The efficiency of AOPs can be enhanced with suitable catalysts and the implementation of hybrid processes, such as UV/photocatalysis, UV-Fenton, and photo-Fenton [12]. These strategies offer promising prospects to enhance the efficiency of wastewater treatments, particularly in the textile industry.

The photo-Fenton method involves the activation of hydrogen peroxide in the presence of iron and ultraviolet light, generating highly reactive hydroxyl radicals. Its efficacy has been demonstrated in treating textile wastewater, showcasing its ability to decompose resistant dyes and persistent organic compounds [13]. The key lies in its efficiency in triggering advanced oxidation reactions, achieving a more comprehensive degradation of contaminants, which can further be optimized through careful selection of catalysts and manipulation of reaction conditions [14].

In the specific context of the textile industry, photo-Fenton emerges as a promising tool to address the complexity of dyes and chemicals present in effluents, as its application not only aims for efficient decolourization but also contributes to reducing the total pollutant load, thereby mitigating the environmental impact associated with textile waste [15]. This approach offers an innovative and sustainable solution to improve the efficiency of wastewater treatments, aligning with the necessity for more environmentally responsible practices. In this manner, the following research aims to achieve the decolourization of wastewater from the artisanal textile industry through the photo-Fenton method, based on its capacity, thereby contributing to the evolving understanding and development of sustainable solutions in wastewater treatment.

MATERIALS AND METHODS

In the experimental setup and fading test procedure section (Figure 1), the following equipment was utilized: a colourimeter, Elettronica Veneta brand, model EVS-BIO-05/EV; a datalogger, Elettronica

Veneta brand, model EV2010/EV; an analytical balance, Sartorius brand, model A2214, with a capacity of 220 g and a precision of ± 0.1 mg; a pH meter, SI Analytics brand, model HandyLab 600; a stopwatch; a magnetic stirrer with a digital heating plate, JKI brand, model MI0102005; and a Lenovo personal computer.

Initially, the preparation of synthetic textile wastewater was conducted by dissolving 40 mg of green aniline in 1 L of water to achieve a concentration of 40 mg/L. The solution was vigorously shaken until homogenized. It is worth noting that this concentration was determined based on various studies, considering the availability of different types of aniline in the market. For instance, [16], [17], and [18] investigated low levels ranging from 1.83 to 30 mg/L, while [18], [19], and [20] examined higher concentrations ranging from 150 to 280 mg/L. The results of these studies showed inconsistency regarding the optimal initial concentration for achieving greater degradation.

Subsequently, to determine the concentrations of Fe^{2+} , H_2O_2 , and treatment time required for decolourization of the residual water, the sample beaker was placed on a magnetic stirrer, exposed to solar rays, and stirred at 1000 rpm. Distilled water was added until the volume reached 1 L (refer to Figure 1).



Figure 1. Experimental setup and decolourization testing procedure

The pH level maintained throughout the experiment was 3, adjusted using drops of H_2SO_4 . Subsequently, ferrous sulfate (at concentrations of 50 and 150 mg/L) was weighed, and the volume of the H_2O_2 solution (at concentrations of 0.5 and 1.0 g/L) was measured and added to the beaker according to the experimental design matrix. Samples were then collected after 1, 2, or 3 hours to measure the absorbance using a colourimeter for each sample, as outlined in Table 1.

Table 1. Analytical techniques for collecting specific data

Variables or parameter	Specific techniques
Dye concentration	Spectroscopy
pH	Potentiometry
Weight	Gravimetry

Finally, to determine the concentration of aniline after the photo-Fenton treatment, it was necessary to establish a calibration curve. To accomplish this, solutions at various concentrations (0, 4, 8, 12, 16, 20, 24, 28, 32, and 36 mg/L) were prepared from the aniline matrix solution in 100 mL vials. This involved measuring 0, 10, 20, 30, 40, 50, 60, 70, 80, and 90 mL, respectively, to fill the vials to 100 mL. Absorbance readings were then taken using a colourimeter for all solutions, including distilled water.

RESULTS AND DISCUSSION

In this research, a randomized block factorial design was employed due to the consideration of three study variables. Two variables were assessed at two levels each, while one variable had three levels, resulting in a 2×2×3 design as depicted in Table 2.

Table 2. Design matrix

N°	Fe2+ concentration (mg/L)	H ₂ O ₂ concentration (g/L)	Treatment time (h)
1	50	0.5	1
2	50	0.5	2
3	50	0.5	3
4	50	1.0	1
5	50	1.0	2
6	50	1.0	3
7	150	0.5	1
8	150	0.5	2
9	150	0.5	3
10	150	1.0	1
11	150	1.0	2
12	150	1.0	3

For the hypothesis test, an analysis of variance (ANOVA) was conducted to establish the relationship between the concentrations of Fe²⁺, H₂O₂, and treatment time, as presented in Tables 5, 6, and 7, respectively.

Table 5. Normality tests

		Kolmogorov-Smirnova			Shapiro-Wilk		
		Statistic	gl	Sig.	Statistic	gl	Sig.
Decolourization of textile wastewater (%)	Fe ²⁺ concentration						
	50 mg/L	0.185	12	0.200*	0.883	12	0.095
	150 mg/L	0.206	12	0.168	0.862	12	0.052
	Concentration H ₂ O ₂						
	0.5 g/L	0.160	12	0.200*	0.929	12	0.372
	1.0 g/L	0.165	12	0.200*	0.931	12	0.389
	Treatment time						
	1 h	0.174	8	0.200*	0.937	8	0.581
	2 h	0.171	8	0.200*	0.889	8	0.231
	3 h	0.248	8	0.160	0.867	8	0.140

Since the asymptotic significance for the concentration of Fe²⁺, H₂O₂, and treatment time is greater than 0.05, we cannot reject the null hypothesis (indicating that interaction effects are not present). Therefore, we conclude that the independent variables analyzed follow a normal distribution.

Table 6. Homogeneity of variance test

Decolourization of textile wastewater					
		Based on the mean	It is based on the median	It is based on the median and with adjusted gl	It is based on the trimmed trimmed mean
Concentration Fe ²⁺	Statistic Levene's	0.008	0.007	0.007	0.008
	df1	1	1	1	1
	df2	14	14	13.145	14
	Sig.	0.931	0.936	0.936	0.932
Concentration H ₂ O ₂	Statistic Levene's	0.008	0.007	0.007	0.008
	df1	1	1	1	1
	df2	14	14	13.145	14
	Sig.	0.931	0.936	0.936	0.932
Treatment time	Statistic Levene's	0.008	0.007	0.007	0.008
	df1	1	1	1	1
	df2	14	14	13.145	14
	Sig.	0.931	0.936	0.936	0.932

For the analysis of homogeneity of variances, the asymptotic significance for the concentrations of Fe^{2+} , H_2O_2 , and treatment time is greater than 0.05. Therefore, it is concluded that the independent variables analyzed exhibit homogeneity of variances.

Table 7. Analysis of variance

Origin	Sum of squares	gl	Quadratic mean	F	Sig.
Corrected model	14723.084 ^a	11	1338.462	265.30	0.000
Intersection	90547.575	1	90547.575	17947.87	0.000
Concentration Fe^{2+}	810.263	1	810.263	160.61	0.000
Concentration H_2O_2	16.733	1	16.733	3.32	0.094
Treatment time	13805.174	2	6902.587	1368.20	0.000
Concentración de Fe^{2+} × Concentration H_2O_2	11.147	1	11.147	2.21	0.163
Concentration Fe^{2+} × Treatment time	6.074	2	3.037	0.60	0.563
Concentration H_2O_2 × Treatment time	14.480	2	7.240	1.43	0.276
Concentration Fe^{2+} × Concentration H_2O_2 × Treatment time	59.212	2	29.606	5.87	0.017
Error	60.540	12	5.045		
Total	105331.199	24			
Total corrected	14783.624	23			

a. $R^2 = 0.996$ (Adjusted $R^2 = 0.992$)

The asymptotic significance is less than 0.05 for the variables concentration of Fe^{2+} and treatment time. Consequently, the interaction of Fe^{2+} concentration × H_2O_2 concentration × treatment time exhibits significant differences, indicating their influential role in the decolourization process of artisanal textile wastewater using the photo-Fenton method. Conversely, since the significance is greater than 0.05, the variable concentration of H_2O_2 and the interaction of Fe^{2+} concentration × H_2O_2 concentration, Fe^{2+} concentration × treatment time, and H_2O_2 concentration × treatment time do not influence the decolourization of artisanal textile wastewater through the photo-Fenton process.

Calibration curve

To ascertain the final concentration of green aniline in the various experiments, a calibration curve was plotted (Figure 2). This curve correlates the measured absorbance obtained from the colourimeter with the initial concentration of aniline.

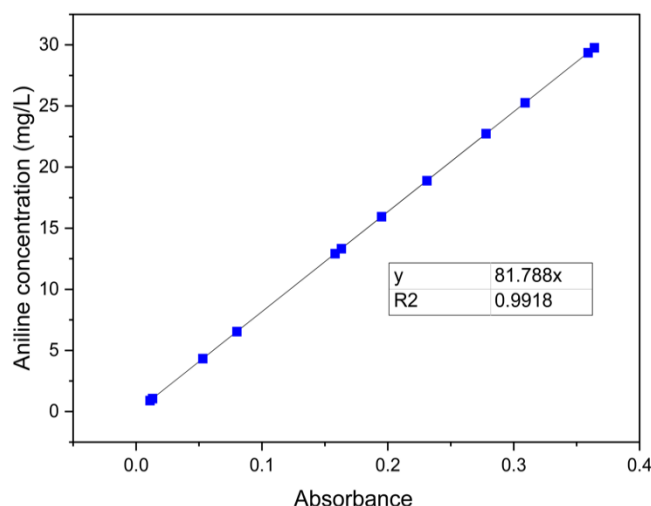


Figure 2. Calibration curve

The calibration curve plays a crucial role in determining the concentration of green aniline in experiments, as it establishes a quantitative relationship between the absorbance measured in the colourimeter and the known concentration of the aniline. Without this curve, assigning concentration values to absorbance readings would be impossible, making it difficult or even impossible to determine the concentration of aniline in the samples.

Aniline concentration after photo-Fenton treatment

Table 3 illustrates that when the initial concentration of the pollutant is relatively low, a higher degradation occurs, attributed to the increased production of $\bullet\text{OH}$ radicals. Conversely, in situations with higher concentrations, inhibition of the H_2O_2 reaction may occur, resulting in lower degradation, as indicated by [17]. Furthermore, the concentration of Fe^{2+} (photocatalyst) significantly influences the degradation rate of the dye (pollutant). It is evident that at a concentration of 150 mg/L, the decolourization surpasses that obtained at 50 mg/L. However, it is emphasized that determining the optimal condition experimentally is crucial due to the variability in wastewater and contaminant characteristics.

Nevertheless, it is important to note that excessively high levels of Fe^{2+} can hinder aniline degradation, as observed by [17]. Additionally, [1] mentions that dilute Fe^{2+} may suppress aniline degradation. Moreover, [2] points out that H_2O_2 accelerates the corrosion of $\text{Fe}(\text{O})$ and generates nanoscale iron hydroxides. Consequently, aniline is initially degraded with OH , followed by the removal of degradation products by iron hydroxides through adsorption and coprecipitation. On a different note, [3] utilized an iron-carbon internal circulation microelectrolysis reactor to almost completely degrade aniline. They investigated the effects and optimization of reaction time, initial pH, aeration rate, and Fe/C ratio

on the aniline removal rate, achieving a reduction to 0.26 mg/L under optimal conditions, with a Fe/C ratio of 1:2.

Table 3. Final concentration depending on the concentration of Fe²⁺ and H₂O₂ and treatment time

N°	Fe ²⁺ concentration (mg/L)	H ₂ O ₂ concentration (g/L)	Treatment time (h)	Absorbance		Aniline concentration (mg/L)	
				I	II	I	II
1	50	0.5	1	0.359	0.347	29.362	28.380
2	50	0.5	2	0.195	0.231	15.949	18.893
3	50	0.5	3	0.080	0.095	6.543	7.770
4	50	1.0	1	0.364	0.377	29.771	30.834
5	50	1.0	2	0.231	0.213	18.893	17.421
6	50	1.0	3	0.053	0.060	4.335	4.907
7	150	0.5	1	0.309	0.321	25.272	26.254
8	150	0.5	2	0.163	0.179	13.331	14.640
9	150	0.5	3	0.013	0.021	1.063	1.718
10	150	1.0	1	0.278	0.289	22.737	23.637
11	150	1.0	2	0.158	0.168	12.923	13.740
12	150	1.0	3	0.011	0.013	0.900	1.063

Percentage of decolourization after photo-Fenton treatment

Similarly, concentration evaluations of the wastewater decolourization percentage estimates were conducted and are presented in Table 4. Thus Fe²⁺ concentrations of 50 and 150 mg/L yielded decolourization rates of 55.612% ± 7.347% and 67.234% ± 7.204%, respectively. It is noteworthy that these concentrations align with similar results obtained by [22] and [23], who investigated Fe²⁺ levels of 100 and 224 mg/L in their respective studies. This concentration directly correlates with the characteristics and concentration of the pollutant, influencing the generation of •OH radicals and, consequently, the efficiency of the process.

Regarding the treatment duration of 1, 2, and 3 hours, the decolourization rates were 32.422% ± 2.649%, 60.691% ± 2.157%, and 91.1567% ± 2.401%, respectively.

Table 4. Percentage of decolourization

N°	Fe ²⁺ concentration (mg/L)	H ₂ O ₂ concentration (g/L)	Treatment time (h)	Textile residual water decolourization (%)		
				I	II	Average
1	50	0.5	1	26.595	29.049	27.822
2	50	0.5	2	60.128	52.767	56.448
3	50	0.5	3	83.642	80.575	82.109

N°	Fe ²⁺ concentration (mg/L)	H ₂ O ₂ concentration (g/L)	Treatment time (h)	Textile residual water decolourization (%)		
				I	II	Average
4	50	1.0	1	25.573	22.915	24.244
5	50	1.0	2	52.767	56.448	54.608
6	50	1.0	3	89.163	87.732	88.447
7	150	0.5	1	36.819	34.365	35.592
8	150	0.5	2	66.671	63.400	65.036
9	150	0.5	3	97.342	95.706	96.524
10	150	1.0	1	43.157	40.908	42.033
11	150	1.0	2	67.694	65.649	66.671
12	150	1.0	3	97.751	97.342	97.546

During the investigation, the optimal conditions for Fe²⁺ concentration, H₂O₂ concentration, and treatment time were determined to be 150 mg/L, 1.0 g/L, and 3 hours, respectively. Under these conditions, the decolourization of the textile wastewater reached a remarkable 97.546%. This result is comparable to that achieved by [23], who attained a 95% decolourization rate. However, it should be noted that in their study, they utilized higher levels of the variables and a different initial concentration of aniline.

Additionally, three levels were considered, based on the observations of Gürses et al. [4]. In their study on optimizing the photo-Fenton process for wastewater decolourization, they noted that varying the evaluation times allowed for a comprehensive understanding of the decolourization kinetics. The authors concluded that interactions among the factors influencing process efficiency can be evaluated with a small number of experiments, eliminating the need for high costs associated with experimentation and result analysis.

The conducted research exhibits unique characteristics. To begin with, the materials and equipment utilized were low-cost and readily available for all experimental procedures, ensuring accessibility to the researchers at all times. Furthermore, it is noted that generally, when the initial concentration of the contaminant is relatively low, degradation is more pronounced due to the higher production of -OH radicals. Conversely, at higher concentrations, the reaction of H₂O₂ in the redox-active centres may be inhibited, as highlighted by [17]. Additionally, a significant amount of ultraviolet (UV) light can be absorbed by the pollutant molecules rather than the catalyst, potentially diminishing efficiency and catalytic activity, as indicated by the same authors.

The photo-Fenton (photocatalytic) process necessitates a level of energy supplied by UV light, typically ranging from wavelengths of 100 to 400 nm, for various photocatalytic chemical reactions. Hence, in studies, artificial UV light is often employed, although there is a growing trend towards utilizing solar

radiation as a natural source. Several researchers underscore the importance of leveraging solar radiation as a UV energy source, including [24–26].

During the experimental phase of the thesis, tests were conducted on sunny days to ensure the availability of UV light. However, due to the energy from other wavelengths contained in solar rays, there was a slight increase in temperature during treatment. It is noteworthy that this factor positively influenced the decolourization of the dye.

CONCLUSION

The application of the photo-Fenton process for decolorizing synthetic wastewater related to the artisanal textile industry has emerged as a promising and efficient strategy. Through this research, a deeper understanding of the reaction mechanisms involved in this advanced oxidation process, as well as the influence of key factors, has been achieved. It has been established that the concentration of Fe^{2+} , treatment time, and the interaction of Fe^{2+} concentration \times H_2O_2 concentration \times treatment time significantly impact the degree of decolourization. Conversely, the concentration of H_2O_2 and other interactions do not exert a significant influence on the process. Optimal conditions were found to be 150 mg/L for Fe^{2+} concentration, 1.0 g/L for H_2O_2 concentration, and 3 hours for treatment time. Moreover, the highest percentage of decolourization of the residual water achieved was 97.546% for the sample with an initial concentration of 40 mg/L. However, it should be noted that this percentage may vary depending on factors such as the initial concentration, type of dye, or contaminant present in the sample. Lastly, the initial concentration level of the dye was found to be directly related to the concentration of Fe^{2+} and H_2O_2 , treatment time, and the degree of decolourization of the wastewater.

Author Contributions

Conceptualization – Huaman K, Lozano A; methodology – Huaman K, Lozano A and Navarro N; formal analysis – Huaman K, Lozano A, Navarro N and Ortega K; investigation – Huaman K, Lozano A, Navarro N and Ortega K; resources – Huaman K; writing-original draft preparation – Lozano A, Ortega K; writing-review and editing – Huaman K and Navarro N, Lozano A, Ortega K; visualization – Lozano A, Ortega K; supervision – Huaman K. All authors have read and agreed to the published version of the manuscript.

Conflicts of Interest

The authors declare no conflict of interest.

Funding

This research received no external funding.

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